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(21) International Application Number: PCT/US88/00227 (22) International Filing Date: 27 January 1988 (27.01.88) (31) Priority Application Number: 074,635 (32) Priority Date: 17 July 1987 (17.07.87) (33) Priority Country: US (71) Applicant: BRUNSWICK CORPORATION [US/US]; One Brunswick Plaza, Skokie, IL 60077 (US). (72) Inventors: WRASIDLO, Wolfgang, J. ; 307 Prospect Street, LaJolla, CA 92037 (US). HOFFMAN, Frieder, K. ; 2630 Autumn Drive, Oceanside, CA 92056 (US). MYSELS, Karol, J. ; 8327 LaJolla Scenic Drive, La- Jolla, CA 92037 (US).		(74) Agent: GREIF, Arthur; Brunswick Corporation, 2000 Brunswick Lane, DeLand, FL 32724 (US). (81) Designated States: AT (European patent), AU, BE (Eu- ropean patent), CH (European patent), DE (Euro- pean patent), DK, FR (European patent), GB (Euro- pean patent), IT (European patent), JP, KR, LU (Eu- ropean patent), NL (European patent), SE (European patent), SU. Published <i>With international search report.</i>
(54) Title: POLYTETRAFLUOROETHYLENE COATING OF POLYMER SURFACES (57) Abstract Adherent, PTFE coatings on polymer surfaces can be produced at temperatures well below the sintering temperature of PTFE, by contacting the surface with a dilute dispersion of PTFE particles and heating the surface to its softening point (in the vicinity of its glass transition temperature) to dry it and to cause the individual particles to become embedded in and surrounded by the polymer.		

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POLYTETRAFLUOROETHYLENE COATING OF POLYMER SURFACESTechnical Field

This invention relates to a method for coating polymer surfaces with fluoroplastics, and is particularly related to a method for increasing the water repellency of such surfaces by coating with dispersions of polytetrafluoroethylene polymers.

Background Art

Fluoroplastics are known to offer a unique combination of chemical, electrical, and mechanical properties which makes them useful over a broad range of applications. One such fluoroplastic, polytetrafluoroethylene (PTFE), exhibits exceptional resistance to chemicals. Aqueous dispersions of PTFE have been used to impregnate fabrics to impart hydrophobic properties and resistance to chemicals, as shown, for example, in U.S. Patent 4,342,675. PTFE coatings are most commonly achieved by contacting the surface to be coated with a dispersion containing about 45-50% solids, drying, and heating the resin particles to temperatures of 357-400°C to cause the particles to sinter and thereby bond to the surface. It has also been suggested that coatings with a degree of useful properties can be achieved at temperatures below that of the sintering temperature of TFE resin particles by either: (i) spray-coating the polymer surface with a volatile solvent for the polymer, sufficient to soften the surface, causing it to become tacky and thereby penetrable by the PTFE particles, as shown in U.S. Patent 3,200,006; (ii) the use of pressure to embed the particles into the substrate, see for example DuPont Product Information Bulletin No. X-50G; or (iii) the use of chemical coupling agents (heavy metal organic complexes) which are capable of bonding both to the PTFE particles and the surface to be coated, see U.S.

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Patents 3,968,297 and 4,232,087. However, these procedures will be of limited value for those substrates in which the dissolution thereof, the use of compressive forces, or the use of contaminating chemicals would be a serious detriment to the coated surface, e.g., for membranes employed in filtration and medicinal applications.

Disclosure of Invention

It has now been found that a substantial degree of hydrophobicity can be imparted to polymer surfaces, whether in the form of cast films or membranes, or woven or nonwoven fabrics, by coating such surfaces with aqueous dispersions of PTFE homopolymers or TFE copolymers utilizing: (i) temperatures within a narrow range, to achieve a novel type of bonding between the substrate and the coating particles; preferably in combination with (ii) dispersions having a dilution about an order of magnitude lower than has most commonly been employed; and (iii) wetting agents which can be evaporated at temperatures below that at which bonding of the particles is effected. Thus, the invention comprises the use of aqueous PTFE dispersions (in which the particles are essentially within the range 0.05 to 3 μ m, preferably 0.1 to 0.5 μ m) containing a volatile wetting agent and having a solids content of 0.1 to 6 percent, preferably 0.3 to 1 percent, wherein such dispersions are contacted with the surface to be coated, which is then heated both to evaporate the wetting agent and to achieve softening or segmental mobility. Once the wetting agent has been removed, the resulting softening permits the molecules of the surface to be drawn around the base of the particles, to produce a bond which has been found to provide an adherent coating which exhibits a superior degree of hydrophobicity. The above method can be employed with any polymer which exhibits a transformation from a solid to a more or

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less viscous liquid state over a comparatively broad temperature range -- rather than the abrupt change associated with purely crystalline materials. With the exception of a few materials (e.g., melamine and silicone), most polymers exhibit such a transformation, known as the glass transition, in which the polymer viscosity decreases rapidly as temperature is increased. Surface softening is generally associated with the onset of that transformation. To the extent that requisite surface softening is achieved, the bonding mechanism of this invention could be employed up to the temperature (357°C) at which the PTFE particles will sinter. However, because it can provide bonding while avoiding surface degradation, the instant method will be of particular benefit in coating polymers: (i) which exhibit softening at temperatures below 250°C, and more generally below 200°C; and (ii) in the absence of substantial compressive force, i.e., pressure of a degree which would cause the particles to be embedded -- absent softening of the polymer surface.

Modes for Carrying Out the Invention

Although PTFE coatings are known to enhance chemical resistance, the principal objective of the instant invention is to impart hydrophobic or anti-wetting properties to the polymer surfaces. Initial trials were conducted by coating a commercially available polysulfone filtration membrane. To prevent destruction or degradation of the pores of this membrane, experimentation was conducted to determine if adherence could be achieved at temperatures well below that at which actual flow (T_m) was encountered. For polysulfone, it was determined that a temperature of 180°C was sufficient to achieve a desirable degree of surface softening. It should be noted that this temperature is somewhat below the glass transition temperature, T_g , of

polysulfone, variedly reported to be, for example, 187°, 190°, and 195°C in the literature. Hydrophobicity, i.e., the degree of adhesion of water droplets to the coated surface, was determined by the visual observation and characterization of the contact angle, i.e., the degree of beading, of small water droplets on the coated surface. Using such visual observation, the degree of hydrophobicity imparted could be set forth in three categories: (I) "superior" -- in which the contact angle was very steep, i.e., of the order of 90°; (II) "satisfactory" -- in which the contact angle was of the order of 45°; and (III) "unsatisfactory" -- those in which the contact angle was markedly shallow.

The dip coating of the polysulfone membrane with a commercial PTFE dispersion (TEFLON 30, sold by DuPont Company, Wilmington, Delaware, containing about 60 percent solids and about 6 percent of a wetting agent) proved comparatively ineffective in imparting hydrophobic properties. Utilizing Scanning Electron Micrographs (SEM), it was determined that lower PTFE solids concentrations would produce a discontinuous, monolayer of adherent particles which exhibited enhanced hydrophobicity in comparison with the essentially continuous, smooth layer of particles, which resulted from the use of the high PTFE concentrations. A set of experiments was run in which the TEFLON 30 was diluted with: (a) an aqueous solution containing 0.5 percent perfluorooctanoic acid (PFOA) neutralized with ammonium hydroxide (rather than NaOH so as to maintain requisite volatility) to a pH of 7.3; and (b) an aqueous solution of 16 percent isopropanol, to produce dispersions of varying solids content. The polysulfone membranes were soaked in the PTFE dispersions for about one second and thereafter heated to 180°C, both to evaporate the

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wetting agent and soften the surface. The results are reported in the Table below:

TABLE

(a) wetting agent -- PFOA neutralized to pH of 7.3

5	<u>PTFE Solids concentration (%)</u>	<u>Hydrophobicity</u>
	0.3	II
	0.42	I
	0.54	I
10	0.66	II
	0.78	II

(b) wetting agent -- isopropanol

15	<u>PTFE Solids concentration (%)</u>	<u>Hydrophobicity</u>
	0.2	II
	0.4	II
	0.8	I
	1.6	I
20	3.2	I

It is seen from the results above, utilizing a temperature, 180°C, far below that suggested in the literature (for dispersions devoid of organo-metallic complexes to achieve bonding), that "superior" hydrophobicity could be achieved by utilizing dilute dispersions of PTFE particles in which the optimum solids concentration is, to some extent, a function of the wetting agent employed. Thus, with PFOA at a pH of 7.3, superior anti-wetting is achieved in a narrow concentration range of about 0.5 percent PTFE particles; while, for the isopropanol wetting agent, the optimum solids concentration would be about 1-3 percent.

For those end-uses in which melting of the polymer surface would be detrimental, it is, of course, necessary that the surface be heated to a temperature well below

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the melting point (T_m) of the polymer. The maximum temperature at which the surface should be heated will depend largely on the degree of surface degradation which can be tolerated. Even in those instances in which a substantial degree of degradation is tolerable, there will be little need to maintain the temperature of the surface at a value more than 20°C above the softening point, to achieve a desired degree of bonding. Generally, such bonding will be achieved with a temperature no more than 10°C thereabove. In any event, the surface must, however, be heated to a temperature high enough and long enough to evaporate the wetting agent and to achieve a sufficient degree of softening or segmental mobility, whereby the colloidal PTFE particles can become embedded into the surface. Scanning Electron Micrographs (SEM) suggest that an intermolecular type of force, such as van der Waals interaction, appears to draw the surface molecules (capable of movement at the "softening" temperature) around the base of each particle. The enhanced bonding apparently results from attraction between the enlarged contact area of the two surfaces, i.e., the coated polymer surface which is in contact with and surrounds the surface quadrant of the PTFE particle embedded therein.

The specific temperature at which optimum "softening" will occur for each polymer cannot be predetermined with complete specificity; although it will generally be in the vicinity of T_g -- the glass transition temperature. However, use of T_g 's variedly reported in the literature for a particular polymer may, in some instances, be insufficient to achieve the segmental mobility necessary to achieve the desired adherence; while in many instances, the reported T_g may be too high and detrimental to the surface. Thus, T_g can vary not only with the structural and morphological parameters (e.g.,

degree of substitution, molecular-weight distribution, degree of chain entanglement) of a given polymer, but also with the experimental parameters (heating and/or penetration rate) employed in its determination.

- 5 Therefore, for any given polymer surface and heating method to be employed, it will be preferable to determine, empirically, the requisite surface "softening" temperature, at which segmental mobility is sufficient to permit the molecules of the surface to be drawn around the base of
- 10 the PTFE particles. In this regard, it must be borne in mind that such surface-particle interaction can only occur after the wetting agent has evaporated. The above notwithstanding, T_g can nevertheless serve as a guide, or starting point, in determining the optimum
- 15 "softening" temperature -- particularly when T_g has been determined by measuring volume expansion (at conventional heat-up rates) of the polymer as a function of temperature, such that T_g is the temperature at which the volume expansion coefficient shows an abrupt
- 20 change. Requisite softening will generally be achieved by heating the polymer surface to a temperature below the T_g determined by the above volume expansion procedure.

CLAIMS

1. In the coating of polymer surfaces to impart an adherent coating of polytetrafluoroethylene (PTFE) resin to the surface, wherein a dispersion of PTFE-
5 containing particles within the range 0.05 to $3.0\mu\text{m}$ is deposited on the surface, and the surface is thereafter heated to volatilize the liquids in said dispersion and cause the particles to adhere to the surface,
the improvement for coating polymer surfaces
10 which exhibit a glass transition and soften at temperatures below 250°C , which comprises: (i) providing a dispersion, consisting essentially of PTFE particles having a solids content within the range 0.1 to 6.0% , dispersing agents sufficient to maintain the particles in suspension,
15 and wetting agents to permit the uniform distribution of the particles on the surface, said dispersion being essentially devoid of heavy metal organic complexes; (ii) depositing the dispersion on the surface; and (iii) heating the polymer surface to a temperature at least
20 equal to, but not more than 20°C above, its "softening" temperature, and maintaining the surface at said temperature for a time sufficient to permit said particles to be embedded therein so as to produce an essentially discontinuous, monoparticulate coating of said particles
25 thereon.
2. The method of Claim 1, in which said coating is conducted in the absence of substantial compressive force.
3. The method of Claim 2, in which the surface
30 to be coated softens at temperatures below 200°C .
4. The method of Claim 3, in which said surface is a porous membrane and said particles are within the range 0.1 to $0.5\mu\text{m}$.

5. The method of Claim 4, in which said surface heating temperature is not more than 10°C above the "softening" temperature.

6. The method of Claim 5, in which said dispersion:

- 5 (a) contains a non-ionic or anionic wetting agent which can be volatilized during said heating; and (b) is devoid of heavy metal organic complexes.


7. The method of Claim 4, in which said surface heating temperature is below the T_g , as determined by
10 volume expansion, of said polymer.

8. The method of Claim 3, in which the content of PTFE particles within said dispersion is within the range 0.3 to 1 percent.

INTERNATIONAL SEARCH REPORT

International Application No. PCT/US 88/00227

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC ⁴ : C 08 J 7/04; B 01 D 13/04		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
IPC ⁴	C 08 J; B 01 D; C 09 D; B 05 D	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸		
III. DOCUMENTS CONSIDERED TO BE RELEVANT *		
Category ⁹	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
A	US, A, 3200006 (V.G. FITZSIMMONS) 10 August 1965 see claims	1
A	US, A, 4416791 (Z. HAQ) 22 November 1983 see claims 1,2,6,7; figure 1; column 3, lines 21-32; column 5, lines 19-26; example 1, lines 50-57	1-3
A	GB, A, 862482 (I.C.I.) 8 March 1961 see claims	1

<p>* Special categories of cited documents: ¹⁰</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date.</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"G" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search 11th May 1988		Date of Mailing of this International Search Report 13 JUN 1988
International Searching Authority EUROPEAN PATENT OFFICE		Signature of Authorized Officer  P.C.G. VAN DER PUTTEN

ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.

US 8800227

SA 20799

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 02/06/88. The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A- 3200006		None	
US-A- 4416791	22-11-83	EP-A, B 0079248	18-05-83
		GB-A, B 2109706	08-06-83
		JP-A- 58087050	24-05-83
		AU-A- 9022682	19-05-83
		CA-A- 1190465	16-07-85
		AU-B- 549230	23-01-86
		DE-A- 3278073	10-03-88
GB-A- 862482		None	

87-274411/39 STANLEY ELEC KK 19.02.86-JP-0341F3 (21.08.87) C03c-17/34 C081-07 C094-03/18 Water repellency treatment of base material - involves roughening plasma-polymerised film formed on surface and applying another film CB7-116528	A82 (A26) SNLE 19.02.86 *J6 2191-447-A	A(10-B, 10-D, 11-B5C, 11-C482, 11-C4D)
<p>The treatment comprises forming a plasma polymerised film on the surface base material; etching the surface of the film to roughen it, and forming another plasma polymerised film on the roughened surface.</p> <p>As the plasma polymerised film, a silicone-contg. or fluorine-contg. polymerised film is used. Hexamethyldisiloxane is used as the monomer gas. As the etching gas, CH₄, Ar, O₂ or a mixed gas of these are used. A capacity coupling type h.f. plasma generator (frequency: 18.56 MP-X) was used.</p> <p>ADVANTAGE - This treatment imparts excellent water repellency to the surface of base material. Such a surface prepd. by the method has a very small coeff. of friction and has excellent heat resistance and chemical resistance. (Spp Dwg.No.0/3)</p>		

87-274412/39 CENTRAL GLASS KK 19.02.86-JP-032634 (21.08.87) C03c-21 Chemically reinforced float glass used for optical disk, etc. - shows strength, surface smoothness and reduced warping deg. without any surface polishing CB7-116529	L01 CENG 19.02.86 *J6 2191-449-A	L(1-D38, 1-L2, 1-L4)
<p>The float glass has surface compressive stress of 25-120 kg/mm² and warping rate of ± 0.4 micro m/cm or less, and is obt'd. by controlling K⁺ diffusion between both surfaces of a float glass board in ion exchange so as to maintain the warping rate of the glass board within that of chemically-unreinforced float glass without surface polishing while keeping good strength.</p> <p>USE - Suitable for use as glass board for optical disk and photomask as well as shield glass of automobile etc.. (Spp Dwg.No.0/0)</p>		

87-274413/39 SUMITOMO ELEC IND KK 15.02.86-JP-031143 (21.08.87) C03c-25/02 G02b-06/44 Optical fibre core mfr. - involves applying coating by extrusion die moulding and then air or water cooling CB7-116530	L01 V07 SUME 15.02.86 *J6 2191-450-A	L(1-F3F)
<p>After optical fibre core is formed by applying secondary coating around optical fibre strand using an extrusion moulding die, the optical fibre core is air or water cooled. Immediately before fibre strand is led into extrusion moulding die, the strand is heated.</p> <p>USE/ADVANTAGE - Heating of optical fibre strand before introducing into the moulding die promotes rigid adhesion between fibre strand and secondary coating. Optical fibre is able to withstand temp. fluctuation of repeated high and low temp. without projection of fibre strand at the end portion of fibre core, or harmful influence for optical connector or associated equipment. (Spp Dwg.No.1/3)</p>		

